

Micro structural and Mechanics properties of Steel Nitrided by Plasma

Belahssen Okba¹, Chala Abdelouahed², Benramache Said², Chabane Fouad³, Bensahal Djamel³,

¹ Mechanic Department, Faculty of Sciences and Technology, University of Tebessa, Algeria

² Materials Science Department, Faculty of Sciences, University of Biskra, Algeria

³ Mechanic Department, Faculty of Sciences and Technology, University of Biskra, Algeria

Abstract. Nitriding treatments of low alloyed steels can be performed only at relatively low temperatures in order to avoid a decrease of corrosion resistance due to nitride layers formation. These conditions promote the formation of the compound layer and diffusion zone, which shows high hardness and good corrosion resistance. In the present paper, the influence of the gas mixture N₂-H₂ in plasma Nitriding process on the micro structural and mechanical characteristics of 32CDV13 steel samples was evaluated. This nuance is used in manufacturing mechanical pieces that are greatly solicited in fatigue. Plasma Nitriding treatments were performed at temperatures in the range 773 K for 4 h. The modified surface layer of the Nitrided samples consists mainly of the γ' and ϵ phases, according to metallographic technique analysis, it seems to be essentially a modification of the austenite matrix. High hardness values are observed in the modified layer with a steep decrease to matrix values.

1 INTRODUCTION

Nitriding is a thermochemical process that is typically used to diffuse nitrogen into ferrous materials. This treatment plays an important role in modern manufacturing technologies [1]. Nitrogen ion processes are well known to improve mechanical, wear and corrosion resistance of steels. Several studies about these improvements in different steels can be found in the literature [2–11].

The basic mechanism of plasma nitriding treatment is a reaction between the plasma and the surface of the metal. In addition, depending on the steel compositions and process parameters, the plasma mass transfer has an effect on the formation and thickness of compound layer and diffusion zone [6].

Plasma nitriding owing to a number of advantages such as a lower process temperature, a shorter treatment time, minimal distortions and low energy use compared to conventional techniques has found wide application in industry [2, 3].

The aim of the present study is to investigate the microstructure and the microhardness of 32CDV13 low alloyed steel treated by ion nitriding process. The gas mixture H₂-N₂ injected into reactor has an effect on microstructure and microhardness of steel.

2 EXPERIMENTAL

A series of experiments were carried out to investigate the plasma nitriding of 32CDV13 low alloyed steel. The chemical composition of 32CDV13 is shown in table 1.

Table 1. The chemical composition of steel 32CDV13.

Elements	C	Si	Mn	Cr	Mo	Ni	V
% mass	0.32	0.31	0.5	3.25	0.44	0.11	0.1

This steel, commonly used for nitriding, presents good toughness. The substrate surface was pre-prepared and polished with 1 μm diamond paste. Specimens were nitrided in a vacuum furnace pumped down to low pressure (10–3 mbar) to minimise the oxygen contamination. The samples temperature is measured using thermocouple. The nitriding parameters were fixed similar to previous works [2].

The samples morphology surfaces were observed by Jeol 5900 Scanning Electron Microscope (SEM). X-ray diffraction analyses with Co K α radiations were performed to determine their structure. The samples microhardness is measured using microhardness tester. The samples morphology surfaces were observed by optical microscopy and scanning electron microscope (SEM). The composition of the nitrided layers was verified by Energy Dispersive Spectroscopy (EDS). The specimens for optical microstructure observation were prepared by chemical etching using 5% hydrofluoric acid solution. The nitrided layers were revealed, at room temperature, by etching the samples with Nital 2% (2% v/v nitric acid in absolute ethanol). X-ray diffraction analyses were obtained by using Co K α tube in Bragg–Brentano geometry in the range from 40° to 110°. Finally, microhardness profiles were measured to confirm the layer thickness and to evaluate its uniformity.

3 RESULTS AND DISCUSSION

3.1. Microstructure

The compound layer thickness and diffusion zone of the plasma nitrided 32CDV13 low-alloy steel depending on the N₂ in the gas mixture are shown in figure 1. It can be observed that thickness of compound layer and diffusion zone increases with increase of N₂ at the gas mixture in plasma, at temperature 773 K and 4 h treatment time.

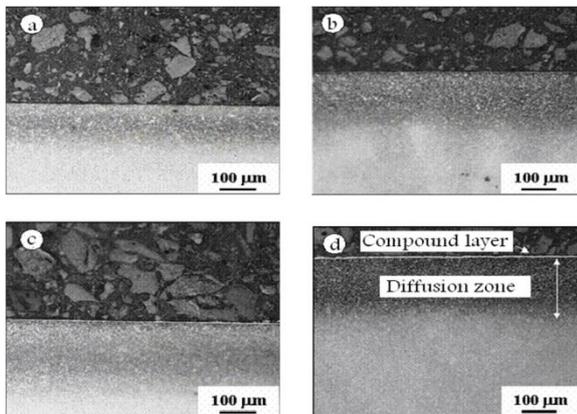


Fig. 1. Optical micrographs plasma nitrided low alloyed steel 32CDV13 at 773 K and 4 h treatment time: (a) 20%N₂, (b) 60%N₂, (c) 80%N₂, (d) 100%N₂.

The micrographic SEM of sample nitrided during 4h in gas mixture (20% H₂ - 80% N₂) at 773 K (Fig. 2) shows the formation of compound layer (white layer) which increases during the process to achieve a thickness around 5 μm. The layer thickness is the most important in this case. The addition of hydrogen in concentration range of 20–40% results in thicker layers and enhanced surface hardness compared with treatment in pure nitrogen. Excessive amounts of hydrogen retard the nitriding process.

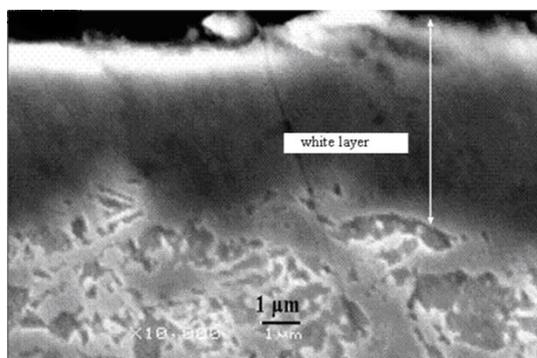


Fig. 2. Micrographic SEM of sample nitrided during 4h in gas mixture (20% H₂ - 80% N₂) at 773 K.

EDS microanalysis showed that the nitrided layer contained a high amount of nitrogen on the surface and the nitrogen concentration decreased along with the

increase of the distance from surface until the substrate value at a depth of about 100–150 μm (Fig.3).

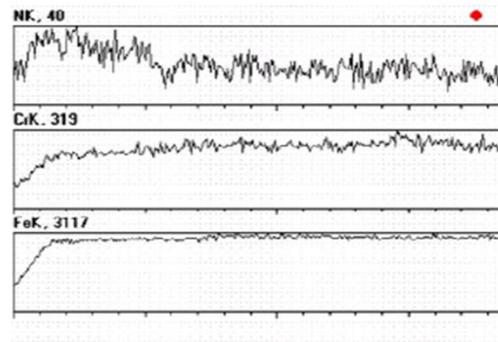


Fig. 3. Concentration profile of elements N, Cr et Fe.

3.2 X-ray Diffraction

Treatment of nitriding by plasma at 773 K and 4 h of treated time produced different nitrided layers in terms of morphology, thickness and phase structure: α phase (corresponding to the steel matrix), the ϵ -Fe₂-3N phase and the γ' -Fe₄N phase. XRD analysis was performed on treated samples (Fig. 4). To demonstrate the effect of the treatment, the diffraction pattern obtained from the untreated material is displayed in the same graph.

When the XRD patterns were examined, it has been seen that both γ' -Fe₄N and ϵ -Fe₂-3N phases have formed and the intensity of this phases in the compound layer is higher in the process, while the N₂ increases in gas mixture.

On increasing nitrogen, the α phase vanishes in thicker nitrided layers, its contribution becomes less intense to the point of disappearing.

The XRD patterns shown in figure 4 indicate that treated samples consist of a mixed structure of γ' -Fe₄N and ϵ -Fe₂-3N. However, the relative peak intensities of the two phases are different in samples with different conditions. It is possible to infer that the presence of ϵ and γ' iron nitrides is determinant to produce the higher hardness.

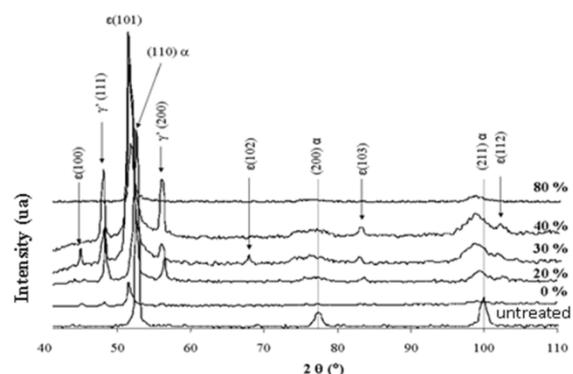


Fig. 4. XRD patterns of samples treated at 773 K for 4 h of treatment at different nitrogen percentage.

3.3 Microhardness

Figure 5 shows microhardness profiles of samples treated at 773 K for 4 h of treatment time at 20/80, 50/50, 60/40, 80/20 and 100/0 of N₂-H₂ gas mixture. Microhardness profiles obtained from cross-sections of treated specimens show the presence of a slope interface between the case (nitrided layer) and the core. All samples show high surface microhardness values that drop decreasingly at the case/core interface to substrate microhardness values. As seen in the figure 4, higher surface hardness values and big depth are obtained at 80% N₂ + 20% H₂ gas mixture. We can see a higher hardness to 100% N₂ in near of the sample surface, but this value decreases to a depth of about 50 μm which explains the role of H₂ in the diffusion of nitrogen in the substrate. These results are in good accordance with those of Krishnaraj et al. [12] who studied the mechanical properties of plasma nitrided steel. Priest and al. [13] studied the effect of hydrogen in the case of nitriding to low pressure of steels. They showed that hydrogen have an effect on the diffusion of nitrogen. Do not include headers, footers, or page numbers other than those already set in this manuscript. Note that the headers, footers or page numbers are different for the first page and the rest of the pages. Actual page numbers and other running heads will be modified when publications are assembled.

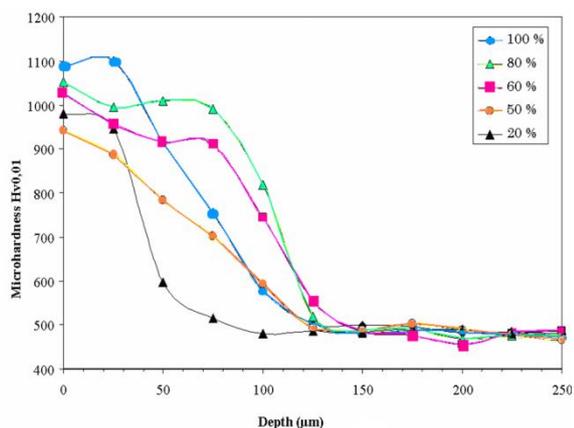


Fig. 5. Micro-hardness profiles of samples treated at 773 K for 4 h of treatment at different nitrogen percentage.

4 Conclusion

The microstructure and mechanical properties of low alloyed steel 32CDV13 nitrided by plasma were studied as a function of concentration of gas mixture. The results obtained show that after 4 hours of treatment and in gas mixture (80% N₂, 20% H₂) at 773K a compound layer and diffusion zone was formed. The compound layer corresponds mainly to Fe₂-3N and Fe₄N iron nitrides and it has been observed that increasing nitrogen in plasma increases significantly the compound layer and

the diffusion zone and improves the mechanical properties.

References

1. C. Nouveau, M.A. Djouadi, P. Beer, P. Jacquet, L. Imhoff, R. Marchal, M. Lambertin, *Duplex Treatment Based on the Combination of Ion Nitriding and PVD Process: Application in Wood Machining*, International Wood Machining Seminar IWMS 15, Los Angeles CA, USA, (2001).
2. C. Nouveau, M.A. Djouadi, L. Chekour, P. Jacquet, M. Lambertin, *Stress Profiles and Thermal Stability of CrxNy Films Deposited by Magnetron Sputtering*, International Conference on Metallurgical Coating and Thin Films ICMTF, San Diego CA, USA, (2002).
3. C. Nouveau, *Déjàs de revêtements durs (Cr_xN_y) obtenus par méthode PVD: réalisation et caractérisations*, Ph.D. thesis, Ecole Nationale des Arts et Métiers, Cluny, France, (2001).
4. T. Gladman, F.B. Pickering, *Grain-Coarsening of Austenite* Journal of the Iron and steel Institute **205**, 653-664, (1967).
5. T. Czerwicz, N. Renevier, H. Michel, *Low-temperature plasma-assisted nitriding*, Surf. Coat. Technol. **131**, 267-277, (2000).
6. D. Manova, S. Mandl, H. Neumann, B. Rauschenbach, *Wear behaviour of martensitic stainless steel after PIII surface treatment*, Surf. Coat. Technol. **200**, 137-140, (2005).
7. J. Barralis, L. Castex, J.C. Chaize, *Genèse des contraintes résiduelles de nitruration Etude expérimentale et modélisation*, Mémoires et Etudes Scientifiques, Revue de métallurgie **43**, 629-642, (1986).
8. J. Pelletier, A. Anders, *Plasma-based ion implantation and deposition*, IEEE Trans. Plasma Sci. **33**, 1944-1959, (2005).
9. F. Borgioli, A. Forsati, E. Galvanetto, T. Bacci, *Glow-discharge nitriding of AISI 316L austenitic stainless steel: influence of treatment temperature*, Surf. Coat. Technol. **200**, 2474-2480, (2005).
10. A.M. Abd El-Rahman, F.M. El-Hossary, F. Prokert, N.Z. Negm, N. Schell, E. Richter, W. Moeller, *In-situ stability study of nitrocarburized 304 stainless steel during heating*, Surf. Coat. Technol. **200**, 602-607, (2005).
11. E. Cano, L. Martinez, J. Simacas, F.J. Perez-Trujillo, C. Gomez, J.M. Bastidas, *Influence of N, Ar and Si ion implantation on the passive layer and corrosion behaviour of AISI 304 and 430 stainless steels*, Surf. Coat. Technol. **200**, 5123-5131, (2006).
12. O. Belahssen, A. Chala, *Comportement en Corrosion Electrochimique de l'Acier Faiblement Allié 32CrMoV13 Nitruré par Plasma*, Annales de Chimie - Science des Matériaux **33**, 423-431, (2008).
13. O. Belahssen, A. Chala, *Microstructure of Low Alloyed Steel 32CDV13 Nitrided by Plasma*, International Journal of Science and Engineering Investigations **1**, 33-24, (2012).

14. N. Krishnara, P. Bala Srinivasan, K.J.L. Iyer, S. Sundaresan, *Optimization of compound layer thickness for wear resistance of nitrocarburized H11 steels*, *Wear* **215**, 123-130, (1998).
15. J.M. Priest, M.J. Baldwin, M.P. Fewell, *The action of hydrogen in low-pressure r.f.-plasma nitriding*, *Surf. Coat. Tech.* **145**, 152-163, (2011).