

# Soret, Dufour and Chemical Reaction Effects on Convective Heat and Mass Transfer over a Stretching Sheet with Heat Generating Sources: A Lie Group Analysis

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## Abstract

In this paper we analysed the effects of Soret, Dufour and Chemical reaction on convective heat and mass transfer of an incompressible, electrically conducting fluid over a stretching sheet in the presence of heat generating sources. The similarity solutions are obtained by using scaling transformations. Furthermore, these similarity equations are solved numerically by using shooting technique with fourth-order Runge-Kutta integration scheme. A comparison with previously published work is performed and the results are found to be in good agreement. Numerical results of the local skin-friction coefficient, the local Nusselt number and the local Sherwood number as well as the velocity, the temperature and the concentration profiles are presented for different physical parameters. The result indicates that (i) for fluids with medium molecular weight ( $H_2$ , air). Dufour and Soret effects should not be neglected (ii) the thickness of concentration boundary layer enhances in the degenerating chemical reaction case and depreciates in the generating chemical reaction case.

**Keywords:** Soret and Dufour effects, Chemical reaction, Heat sources, Stretching sheet, Magnetic field, Scaling transformations, Similarity function and Shooting technique.

## Nomenclature

$a$	parameters of the group
$C_1, C_2, C_3, C_4$	Constants
$C$	concentration of the fluid ( $\text{kgm}^{-2}$ )
$C_p$	specific heat ( $\text{J kg}^{-1} \text{K}^{-1}$ )
$D_m$	coefficient of mass diffusivity ( $\text{m}^2 \text{s}^{-2}$ )
$Du$	Dufour number
$f$	similarity function
$g$	acceleration due to gravity ( $\text{ms}^{-2}$ )
$Gc$	local modified Grashof number
$Gr$	local Grashof number
$k$	chemical reaction parameter
$M$	magnetic parameter
$m$	index parameter
$Nu$	Nusselt number
$Pr$	Prandtl number
$Re_x$	local Reynolds number
$Sc$	Schmidt number
$Sh$	Sherwood number
$Sr$	Soret number
$T$	temperature of the fluid (K)
$T_m$	mean fluid temperature
$U(x)$	stretching speed of the plate ( $\text{ms}^{-1}$ )
$u, v$	the x-and y-component of the velocity field ( $\text{ms}^{-1}$ )
$x, y$	cartesian coordinates (m)
<i>Greek symbols</i>	
$\Psi$	stream function
$\eta$	similarity variable
$\theta$	dimensionless temperature
$\phi$	dimensionless concentration
$\nu$	kinematic viscosity ( $\text{m}^2 \text{s}^{-1}$ )
$\rho$	density ( $\text{kg m}^{-3}$ )
$\tau$	skin-friction
$\alpha$	heat source parameter
$\alpha_l$	thermal diffusivity ( $\text{m}^2 \text{s}^{-1}$ )

$\beta_T$  coefficient of thermal expansion ( $K^{-1}$ )  
 $\beta_c$  coefficient of thermal expansion with concentration ( $kg^{-1} m^3$ )

*Subscripts*

$w$  wall condition  
 $\infty$  free stream condition  
 $o$  constant condition

*Superscript*

$()'$  differentiation with respect to  $\eta$

## 1. Introduction

The study of hydrodynamic flow and heat transfer over a stretching sheet has gained considerable attention due to its application in industry and important bearings on several technological processes. In particular, many metallurgical processes involve the cooling of continuous strips or filaments by drawing them through a quiescent fluid and that in the process of drawing, these strips are sometimes stretched. In the case of annealing and thinning of copper wires, the properties of the final product depend to a great extent on the rate of cooling. By drawing such strips in an electrically conducting fluid subject to a magnetic field, the rate of cooling can be controlled and final products of desired characteristics might be achieved and this has been studied by the authors Chakrabarti et al (1979). And also, in several engineering processes, materials manufactured by extrusion processes and heat treated materials travelling between a feed roll and a wind up roll on convey belts possess the characteristics of a moving continuous surface. The steady flow on a moving continuous flat surface was first considered by Sakiadis (1961) who developed a numerical solution using a similarity transformation. The researchers Ramana Reddy et al. (2014), sulochana et al. (2015), Sugunamma et al. (2014) and Veera Suneela Rani et al. (2012) discussed the radiation effects on convective flows through different channels. The two-dimensional flow caused solely by a linearly stretching sheet in an otherwise quiescent incompressible fluid which has a very simple closed form exponential solution was established by Crane (1970). Gupta and Gupta (1977) studied the heat and mass transfer in a stretching surface with suction or injection. Chen and Char (1998) studied the effects of variable surface temperature and variable surface heat flux on the heat transfer characteristics of a linearly stretching sheet. Gorla et al (1998) studied the MHD effect on a vertical stretching surface with suction and blowing. Seddeek (2007) studied the effects of heat generation or absorption on heat and mass transfer of a visco-elastic fluid with a magnetic field over a stretching sheet. In all of the above mentioned studies the thermal-diffusion and the diffusion-thermo are negligible. The effects of the thermal-diffusion and the diffusion-thermo on the transport of heat and mass has been developed from the kinetic theory of gases by Chapman and Cowling (1952) and Hirshfelder et al (1954) explained the phenomena and derived the necessary formulae to calculate the thermal-diffusion coefficient and thermal-diffusion factor for monoatomic gases or for polyatomic gas mixtures. Kafoussias and Williams (1995) studied the effects of thermal-diffusion and diffusion thermo on steady mixed free-forced convective and mass transfer over a vertical flat plate, when the viscosity of the fluid varies with temperature. Alam et al (2005) studied the effects of Dufour and Soret numbers on unsteady free convection and mass transfer flow past an impulsively started infinite vertical porous flat plate, of a viscous incompressible and electrically conducting fluid, in the presence of a uniform transverse magnetic field. Alam et al (2006) studied the effects of Dufour and Soret numbers on unsteady MHD free convection and mass transfer flow past an infinite vertical porous plate embedded in a porous medium. Raju et al. (2015), Sandeep et al. (2012,2013 &2014) discussed the heat transfer characteristics of MHD flows through different channels. The method has been applied intensively by Pakdemirli (1994), Mukhopadhyay et al (2005) and Layek et al (2007). Mukhopadhyay et al (2012) have discussed lie group analysis of MHD boundary layer slip flow past a heated stretching sheet in presence of heat source/sink. Subhas Abel et al (2013) have investigated MHD flow and transfer of mixed hydrodynamic/thermal slip over a linear vertically stretching sheet. Dulal pal et al (2011) have studied the effect of Soret, Dufour, chemical reaction and thermal radiation on MHD, non-darcy, unsteady mixed convective heat and mass transfer over stretching sheet. Dulal pal et al (2012) have investigated the effects on MHD non-darcian mixed convective heat and mass transfer over a stretching sheet with non-uniform heat source/sink. Lakshminarayana et al (2010) have investigated Soret and Dufour effects on free convection along vertical wavy surface in a fluid saturated darcy porous medium. Ching-Yang-Cheng (2011) have investigated Soret and Dufour effects on free convective boundary layer over inclined wavy surface in a porous medium.

In the risk assessment of nuclear power plants, the possibility and the consequences of a meltdown of the reactor core are usually considered. During the course of such an accident molten fuel and coolant may interact. Violent thermal reaction can dispose the molten fuel into fine particles. These small particles quickly solidify in the coolant and settle on internal structures of the reactor pressure vessel forming a saturated porous bed. The question arises under what conditions the nuclear decay heat can be removed from the particle bed to

the ambient coolant by natural convection. Thus the problem of natural convection in saturated porous layers. This analysis of heat transfer in a viscous heat generating fluid also important in engineering processes pertain to flow in which a fluid supports an exothermal chemical or nuclear reaction or problems concerned with dissociating fluids and this has been studied by Kafoussias et al (1998). Angirasa et al (1997) have assumed the volumetric heat generation as constant. For example a hypothetical core-disruptive accident in a liquid metal fast breeder reactor (I MFBR) could result in the setting of fragmented fuel debris as horizontal surfaces below the core. The porous debris could be saturated sodium coolant and heat generation will result from the radioactive decay of the fuel particulate and this was studied by Christofer Philips (1990). The heat losses from the geothermal system in some cases can be treated as if the heat comes from the heat generating sources and this was analysed by Gebhart et al (1971). Keeping this in view porous medium with internal heat source have been discussed by several authors like Naga Radhika et al (2010). Recently Afify (2009) has studied free convective heat and mass transfer of an incompressible electrically conducting fluid past a stretching sheet in the presence of suction and injection with thermal diffusion (Soret) and diffusion-thermo (Dufour) effects. Ibrahim et al (2005) have discussed Lie group analysis of radiative and magnetic field effects on free convection and mass transfer flow past a semi- infinite vertical flat plate. Kalpakides et al (2004) have studied Symmetry groups and similarity solutions for a free convective boundary layer problem. Sivasankaran et al (2006) have discussed Lie group analysis of natural convective heat and mass transfer in an inclined surface.

In this paper we investigate the Lie-group analysis of Soret, Dufour and chemical reaction effects on convective heat and mass transfer flow over a stretching sheet with heat generating sources. The similarity solutions are obtained using scaling transformations. The similarity equations are solved numerically by using fourth order Range-Kutta integration scheme with shooting method. Numerical results of local Nusselt number and local Sherwood number as well, the velocity, temperature and the concentration profiles are presented for different values of the governing parameters. From this analysis we find that the velocity component enhances in the generating and degeneration of chemical reaction cases for  $|k| \leq 0.5$  and depreciates for higher  $|k| \geq 2.5$ . The thickness of the thermal boundary layer decreases in the degenerating chemical reaction case and enhances in the generating chemical reaction case, while the thickness of concentration boundary layer enhances in the degenerating chemical reaction case and decreases in the generating chemical reaction case.

## 2. Governing equations

Consider the steady free convective heat and mass transfer flow of a viscous, incompressible and electrically conducting fluid past a stretching surface coinciding with the plane  $y=0$ . Keeping the origin fixed two equal and opposite forces are applied along the  $x$ -axis which results in stretching of the sheet and hence, the flow is generated. The non-uniform transverse magnetic field  $B(x)$  is imposed along  $y$ -axis. The induced magnetic field is neglected as the magnetic Reynolds number of the flow is taken to be very small. It is also assumed that the external electric field is zero and the electric field due to polarization of charges is negligible. The temperature and the concentration of the ambient fluid are  $T_\infty$  and  $C_\infty$  and those at the stretching surface are  $T_w(x)$  and  $C_w(x)$  respectively. It is also assumed that the pressure gradient, viscous and electrical dissipation are neglected. The fluid properties are assumed to be constant except the density in the buoyancy terms of the linear momentum equation which is approximated according to the Boussinesq's approximation. Under the above assumptions, the boundary layer form of the governing equations can be written as

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad (1)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B^2(x)u}{\rho} + g\beta_T(T - T_\infty) + g\beta_C(C - C_\infty) \quad (2)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha_1 \frac{\partial^2 T}{\partial y^2} + \frac{D_m K_T}{C_s C_p} \frac{\partial^2 C}{\partial y^2} + Q(T_\infty - T) \quad (3)$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = D_m \frac{\partial^2 C}{\partial y^2} + \frac{D_m K_T}{T_m} \frac{\partial^2 T}{\partial y^2} - k_1(C - C_\infty) \quad (4)$$

The boundary conditions for Eqs. (1)–(4) are expressed as

$$u(x,0) = U(x) = C_1 x^m, v(x,0) = V_w(x) = C_2 x^n, T = T_w(x) = T_\infty + C_3 x^r, C = C_w(x) = C_\infty + C_4 x^r$$

$$u(x, \infty) = 0, T(x, \infty) = T_\infty, C(x, \infty) = C_\infty \quad (5)$$

Where  $u, v$  are the velocity components in the  $x$ - and  $y$ -directions respectively,  $\nu$  is the kinematic viscosity,  $\sigma$  is

the electrical conductivity,  $\rho$  is the density of the fluid,  $\beta_T$  is the coefficient of thermal expansion,  $\beta_C$  is the coefficient of thermal expansion with concentration.  $T_m$  is the mean fluid temperature.  $T$  and  $T_\infty$  are the temperature of the fluid inside the thermal boundary layer and the fluid temperature in the free stream, respectively, while  $C$  and  $C_\infty$  are the corresponding concentrations. Also  $D_m$  is the coefficient of mass diffusivity,  $C_1, C_2, C_3, C_4$  are the constants,  $U(x)=C_1x^m$  is the stretching speed of the plate,  $V_w(x)=C_2x^n$  is the transverse velocity at the surface,  $B(x)=B_0x^s$  is the applied magnetic field,  $C_p$  is the specific heat at constant pressure,  $\alpha_l$  is the thermal diffusivity,  $K_T$  is the thermal-diffusion ratio,  $C_s$  and  $C_\infty$  is the concentration susceptibility.  $Q$  is the coefficient of temperature dependent heat source,  $k_1$  is the chemical reaction co-efficient. The stream function  $\Psi(x,y)$  is defined by  $u = \frac{\partial \Psi}{\partial y}$  and  $v = -\frac{\partial \Psi}{\partial x}$  such that continuity equation (1) is satisfied automatically. We

introduced the following non-dimensional temperature  $\theta = \frac{T - T_\infty}{T_w - T_\infty}$  and non-dimensional concentration

$\phi = \frac{C - C_\infty}{C_w - C_\infty}$  then Eqs. (2)–(4) and boundary condition (5) become

$$\psi_y \psi_{xy} - \psi_x \psi_{yy} - v \psi_{yyy} + \frac{\sigma B_0^2 x^{2s} \psi_y}{\rho} - g \beta_T \theta (T_w - T_\infty) - g \beta_C \phi (C_w - C_\infty) = 0 \quad (6)$$

$$\psi_y ((T_w - T_\infty) \theta)_x - \psi_x ((T_w - T_\infty) \theta)_y - \alpha ((T_w - T_\infty) \theta)_{yy} - \frac{D_m K_T}{C_s C_p} ((C_w - C_\infty) \phi)_{yy} + Q \theta (T_w - T_\infty) = 0 \quad (7)$$

$$\psi_y ((C_w - C_\infty) \phi)_x - \psi_x ((C_w - C_\infty) \phi)_y - D_m ((C_w - C_\infty) \phi)_{yy} - \frac{D_m K_T}{T_m} ((T_w - T_\infty) \theta)_{yy} + k_1 \phi (C_w - C_\infty) = 0 \quad (8)$$

$$\psi_y(x,0) = C_1 x^m, \psi_y(x,0) = -C_2 x^n, \theta(x,0) = 1, \phi(x,0) = 1 \quad \text{and} \\ \psi_y(x,\infty) = 0, \theta(x,\infty) = 0, \phi(x,\infty) = 0 \quad (9)$$

### 3. Group theory analysis and similarity equations

#### Application of one-parameter transformations group:

The first step of the analysis is to introduce the one-parameter transformation group

$$\bar{x} = a^p x, \bar{y} = a^q y, \bar{\psi} = a^d \psi, \bar{\theta} = \theta, \bar{\phi} = \phi, \bar{T} - \bar{T}_\infty = a^e (T - T_\infty), \bar{C} - \bar{C}_\infty = a^z (C - C_\infty) \quad (10)$$

Where 'a' is the parameter of the group, p,q,d,e and z are real constants to be determined, then substituting group transformation (10) into Eqs. (6)–(8) and boundary conditions (9), we get.

$$\bar{\psi}_y \bar{\psi}_{\bar{y}\bar{x}} - \bar{\psi}_x \bar{\psi}_{\bar{y}\bar{y}} + \frac{\sigma B_0^2 \bar{x}^{-2s} \bar{\psi}_y}{\rho} - g \beta_T (\bar{T}_w - \bar{T}_\infty) \bar{\theta} - g \beta_C (\bar{C}_w - \bar{C}_\infty) \bar{\phi} \\ = a^{2d-p-2q} \psi_y \psi_{xy} - a^{2d-p-2q} \psi_x \psi_{yy} - a^{d-3q} v \psi_{yyy} - a^{d+2sp-q} \frac{\sigma B_0^2 x^{2s} \psi_y}{\rho} - a^e g \beta_T (T_w - T_\infty) \theta - a^z g \beta_C (C_w - C_\infty) \phi \quad (11)$$

$$\bar{\psi}_y ((\bar{T}_w - \bar{T}_\infty) \bar{\theta})_x - \bar{\psi}_x ((\bar{T}_w - \bar{T}_\infty) \bar{\theta})_y - \alpha ((\bar{T}_w - \bar{T}_\infty) \bar{\theta})_{\bar{y}\bar{y}} - \frac{D_m K_T}{C_s C_p} ((\bar{C}_w - \bar{C}_\infty) \bar{\phi})_{\bar{y}\bar{y}} + Q (\bar{T}_w - \bar{T}_\infty) \bar{\theta} \\ = a^{d+e-p-q} \psi_y ((T_w - T_\infty) \theta)_x - a^{d+e-p-q} \psi_x ((T_w - T_\infty) \theta)_y - a^{e-2q} \alpha ((T_w - T_\infty) \theta)_{yy} - a^{z-2q} \frac{D_m K_T}{C_s C_p} ((C_w - C_\infty) \phi)_{yy} \\ + Q a^e (T_w - T_\infty) \quad (12)$$

$$\bar{\psi}_y ((\bar{C}_w - \bar{C}_\infty) \bar{\phi})_x - \bar{\psi}_x ((\bar{C}_w - \bar{C}_\infty) \bar{\phi})_y - D_m ((\bar{C}_w - \bar{C}_\infty) \bar{\phi})_{\bar{y}\bar{y}} - \frac{D_m K_T}{T_m} ((\bar{T}_w - \bar{T}_\infty) \bar{\theta})_{\bar{y}\bar{y}} + k_1 (\bar{C}_w - \bar{C}_\infty) \bar{\phi} \\ = a^{d+z-p-q} \psi_y ((C_w - C_\infty) \phi)_x - a^{d+z-p-q} \psi_x ((C_w - C_\infty) \phi)_y - a^{z-2q} D_m ((C_w - C_\infty) \phi)_{yy} - a^{e-2q} \frac{D_m K_T}{T_m} ((T_w - T_\infty) \theta)_{yy} \\ + k_1 a^z (C_w - C_\infty) \phi \quad (13)$$

The boundary conditions

$$\begin{aligned}
 y=0: \bar{\psi}_y - C_1 \bar{x}^{-m} &= a^{d-q} \psi_y - a^{mp} C_1 x^m = 0, \bar{\psi}_x - C_2 \bar{x}^{-n} = a^{d-p} \psi_x + C_2 a^{np} x^n = 0 \\
 (\bar{T}_w - \bar{T}_\infty) - C_3 \bar{x} &= a^e (T_w - T_\infty) - a^{rp} C_3 x^r = 0, (\bar{C}_w - \bar{C}_\infty) - C_4 \bar{x}^{-r} = a^z (C_w - C_\infty) - a^{rp} C_4 x^r = 0 \\
 y \rightarrow \infty: \bar{\psi}_y &= a^{d-q} \psi_y = 0, (\bar{T} - \bar{T}_\infty) = a^e (T - T_\infty) = 0, (\bar{C} - \bar{C}_\infty) = a^z (C - C_\infty) = 0
 \end{aligned} \tag{14}$$

The condition of conformal invariance implies

$$\begin{aligned}
 2d - p - 2q &= d - 3q = d + 2sp - q = e = z \\
 d + e - p - q &= e - 2q = z - 2q = e \\
 d + z - p - q &= z - 2q = e - 2q = z \\
 d - q &= mp, d - p = np, e = rp, z = rp
 \end{aligned} \tag{15}$$

By solving the previous conditions together, we obtain

$$p = \frac{2q}{1-m}, d = \left(\frac{1+m}{1-m}\right)q, s = \frac{m-1}{2}, n = \frac{m-1}{2}, e = z = \frac{2(2m-1)}{(1-m)}q, r = 2m-1 \tag{16}$$

Under the condition in invariant transformation, the group transformation (10) becomes

$$\begin{aligned}
 \bar{x} &= a^{\left(\frac{2}{1-m}\right)q} x, \bar{y} = a^q y, \bar{\psi} = a^{\left(\frac{1+m}{1-m}\right)q} \psi, \bar{T}_w - \bar{T}_\infty = a^{\left(\frac{2(2m-1)}{1-m}\right)q} (T_w - T_\infty), \bar{C}_w - \bar{C}_\infty = a^{\left(\frac{2(2m-1)}{1-m}\right)q} (C_w - C_\infty), \\
 \bar{\theta} &= \theta, \bar{\varphi} = \varphi
 \end{aligned} \tag{17}$$

**Absolute invariants:**

First we find an absolute invariant which is a function of the dependent variable, namely  $\zeta$  and  $\zeta = yx^N$ . For this purpose we write.

$$\bar{x} = Ax, A = a^{\left(\frac{2}{1-m}\right)}, \bar{y} = A^{\left(\frac{1-m}{2}\right)} y, \bar{\psi} = A^{\left(\frac{1+m}{2}\right)} \psi, \bar{T}_w - \bar{T}_\infty = A^{2m-1} (T_w - T_\infty), \bar{C}_w - \bar{C}_\infty = A^{2m-1} (C_w - C_\infty) \tag{18}$$

To establish  $\bar{y}\bar{x}^{-N} = yx^N$ , we have  $\bar{y}\bar{x}^{-N} = yx^N A^{\left(\frac{1-m}{2}\right)N} + N$ . Putting  $\left(\frac{1-m}{2}\right)N + N = 0$ , we get  $\bar{y}\bar{x}^{-N} = yx^N$ .

Since  $N = \frac{m-1}{2}$  and  $\zeta = yx^{\left(\frac{m-1}{2}\right)}$  is an absolute invariant.

We now calculate a second absolute invariant  $f(\zeta)$ , which involves the dependent variable  $\psi$ . Let us assume

$$\text{that } f(\zeta) = \bar{x}^{-L} \bar{\psi}. \text{ Now } \bar{x}^{-L} \bar{\psi} = A^{\left(\frac{1+m}{2}\right)L} x^{-L} \psi$$

Putting  $\left(\frac{1+m}{2}\right)L + L = 0$  we get,  $L = -\left(\frac{1+m}{2}\right)$ . Thus we get the second absolute invariant  $f(\zeta)$  as

$$f(\zeta) = \bar{x}^{-\left(\frac{1+m}{2}\right)} \bar{\psi}, \text{ finally } \bar{\psi} = x^{\left(\frac{1+m}{2}\right)} f(\zeta). \text{ Similarly, we obtained } \bar{T}_w - \bar{T}_\infty = C_3 x^{2m-1}, C_w - C_\infty = C_4 x^{2m-1}. \text{ We have also } \bar{\theta} = \theta(\zeta), \bar{\varphi} = \varphi(\zeta)$$

It can be seen from Eq. (16), that when the sheet is stretched with a speed  $U(x) = C_1 x^m$  there exists as similarity solution to this problem provided

$$B(x) = B_0 x^{\frac{(m-1)}{2}}, V_w = C_2 x^{\frac{(m-1)}{2}} \tag{19}$$

from which the similarity variable and the dependent variables turn out to be of the form

$$\zeta = yx^{\left(\frac{m-1}{2}\right)}, \psi = x^{\left(\frac{m-1}{2}\right)} f(\zeta), \theta = \theta(\zeta), \varphi = \varphi(\zeta), T_w - T_\infty = C_3 x^{2m-1}, C_w - C_\infty = C_4 x^{2m-1}. \tag{20}$$

To avoid the fluid properties appearing explicitly in the coefficients of the equations, we have the following similarity transformations;

$$\eta = y \sqrt{\frac{m+1}{2} \frac{U(x)}{\nu x}}, \psi = \sqrt{\frac{2}{m+1}} \nu x U(x) f(\eta) \tag{21}$$

$$\theta = \theta(\eta) \tag{22}$$

$$\varphi = \varphi(\eta) \tag{23}$$

$$T_w - T_\infty = C_3 x^{(2m-1)}, \quad C_w - C_\infty = C_4 x^{2m-1}. \quad (24)$$

Substituting Eqs. (21)–(24) into the governing Eqs. (6)–(8) and the boundary condition (9), we finally obtain a system of non-linear ordinary differential equations with appropriate boundary conditions :

$$f''' + ff'' - \left(\frac{2m}{m+1}\right) f'^2 - \left(\frac{2m}{m+1}\right) Mf' + \left(\frac{2m}{m+1}\right) Gr\theta + \left(\frac{2m}{m+1}\right) Gc\varphi = 0 \quad (25)$$

$$\left(\frac{1}{Pr}\right) \theta'' - \frac{2(2m-1)}{m+1} \theta f' + f\theta' + Du\varphi'' - \alpha\theta = 0 \quad (26)$$

$$\left(\frac{1}{Sc}\right) \varphi'' - \frac{2(2m-1)}{m+1} f'\varphi + f\varphi' + Sr\theta'' - k\varphi = 0 \quad (27)$$

The boundary conditions are

$$\begin{aligned} f(0) = f_w, \quad f'(0) = 1, \quad \theta(0) = 1, \quad \varphi(0) = 1 \\ f'(\infty) = 0, \quad \theta(\infty) = 0, \quad \varphi(\infty) = 0 \end{aligned} \quad (28)$$

Where primes denote differentiation with respect to  $\eta$ ,  $M = \frac{\sigma\beta_o^2}{\rho c_1}$  is the magnetic parameter,

$Gc = \frac{g\beta_c(C_w - C_\infty)}{c_1^2 x^{2m-1}}$  is the local modified Grashof number,  $Gr = \frac{g\beta_T(T_w - T_\infty)}{C_1^2 x^{2m-1}}$  is the local Grashof

number,  $Pr = \frac{\nu}{\alpha}$  is the Prandtl number,  $Du = \frac{DmK_T(C_w - C_\infty)}{C_p C_s (T_w - T_\infty) \nu}$  is the Dufour number,

$\alpha = \frac{2Q}{c_1(m+1)x^{m-1}}$  is the heat source parameter,  $Sc = \frac{\nu}{D_m}$  is the Schmidt number,

$Sr = \frac{D_m(T_w - T_\infty)}{T_m \nu (C_w - C_\infty)}$  is the Soret number,  $k = \frac{k_1}{C_1 x^{m-1}}$  is the chemical reaction parameter,

$Re_x = \frac{xU(x)}{\nu}$  is the local Reynolds number,  $f_w = \left(-C_2 \sqrt{\frac{2}{(m+1)\nu C_1}}\right)$  is the suction or injection

parameter which is kept constant.

The quantities of physical interest in this problem are the local skin friction coefficient, the local Nusselt number

and the local Sherwood numbers which are defined by  $Cf = \frac{\tau_w}{\left(\frac{\rho U^2(x)}{2}\right)} = 2\sqrt{\frac{m+1}{2}} \frac{1}{Re_x} f''(0)$ ,

$$Nu = \frac{xq_w}{k^*(T_w - T_\infty)} = -\sqrt{\frac{m+1}{2}} Re_x \theta'(0) \quad \text{and} \quad Sh = \frac{xm_w}{D_m(C_w - C_\infty)} = -\sqrt{\frac{m+1}{2}} Re_x \varphi'(0)$$

(29)

Where

$$\tau_w = \mu \left(\frac{\partial u}{\partial y}\right)(x,0), \quad q_w = -k^* \left(\frac{\partial T}{\partial y}\right)(x,0) \quad \text{and} \quad m_w = -D_m \left(\frac{\partial C}{\partial y}\right)(x,0) \quad (30)$$

#### 4. Numerical method for solution

The Eqs. (25)–(27) constitute a highly non-linear coupled boundary value problem of third and second-order. So we develop most effective numerical shooting technique with fourth-order Runge-Kutta integration algorithm. To select  $\eta_\infty$  we begin with some initial guess value and solve the problem with some particular set of parameters to obtain  $f''(0)$ ,  $\theta'(0)$  and  $\varphi'(0)$ . The solution process is repeated with another larger value of  $\eta_\infty$  until two successive values of  $f''(0)$ ,  $\theta'(0)$  and  $\varphi'(0)$  differ only after desired digit signifying the limit of



the boundary along  $\eta$ . The last value of  $\eta_{\infty}$  is chosen as appropriate value for that particular set of parameters. Eqs (25)–(27) of third-order in  $f$  and second-order in  $\theta$  and  $\phi$  have been reduced to a system of seven simultaneous equations of first-order for seven unknowns following the method of superposition Which was given by Hasen (1979). To solve this system we require seven initial conditions whilst we have only two initial conditions  $f'(0)$  and  $f(0)$  on  $f$ , two initial conditions on each on  $\theta$  and  $\phi$ . Still there are three initial conditions  $f''(0)$ ,  $\theta'(0)$  and  $\phi'(0)$  which are not prescribed. Now, we employ numerical shooting technique where these two ending boundary conditions are utilized to produce two known initial conditions at  $\eta=0$ . In this calculation, the step size  $\Delta\eta=0.001$  is used while obtaining the numerical solution with  $\eta_{\max}=11$  and five-decimal accuracy as the criterion for convergence.

## 5. Results and Discussion

By employing one-parameter group theory to analyse the governing equations and the boundary conditions, the two independent variables are reduced by one, consequently the governing equations reduce to a system of non-linear ordinary differential equations with the appropriate boundary conditions. Finally the system of similarity equations (25)–(27) with boundary conditions (28) is solved numerically by using fourth order Range-Kutta integration with shooting method. In order to get a clear insight of the physical problem, the velocity  $f'$ , the temperature  $\theta$  and the concentration  $\phi$  have been discussed by assigning numerical values to the parameters encountered in the problem.

To be realistic, the values of the Schmidt number are chosen for hydrogen ( $Sc=0.22$ ), water vapour ( $Sc=0.6$ ) and ammonia ( $0.78$ ) at temperature  $25^{\circ}c$  and one atmospheric pressure. Prandtl number takes values 0.7, 1, 2 (especially for air  $Pr=0.71$  at temperature  $20^{\circ}c$  and one atmospheric pressure). Due to free convection problem local Grashof number for heat transfer takes value 2 and local modified Grashof number for mass transfer takes value 10. Index parameter ( $m$ ) takes values 0, 1, 2, magnetic parameter takes values 0, 0.5, 1. The values of Dufour and Soret numbers are chosen in such a way that their product is constant provided that the mean temperature  $T_m$  is kept constant as well. Dufour number takes values 0.03, 0.15, 0.60 and Soret number takes values 2, 0.4, 0.1. The heat source parameter ( $\alpha$ ) takes values 2, 4, 6 and the chemical reaction parameter ( $k$ ) takes values  $\pm 0.5$ ,  $\pm 1.5$ ,  $\pm 2.5$ .

The variation of  $f'$ ,  $\theta$  &  $\phi$  with heat source parameter  $\alpha$  is shown in figs 1-3. It is found from Fig.1 that increase in  $\alpha$  enhances  $|f'|$  at  $\eta=0$ . From Fig.2 we find that an increase in  $\alpha$  enhances the actual temperature at  $\eta=0$ . From Fig.3 we find that the actual concentration depreciates with increase in  $\alpha$  at  $\eta=0$ . Figs 4-6 represent the variation of  $f'$ ,  $\theta$  &  $\phi$  with increase in Dufour parameter  $Du$  (or decrease in Soret parameter  $Sr$ ). It is observed that the velocity component and temperature enhance while the concentration reduces with increase in Dufour parameter (or decreases in Soret parameter). The thickness of temperature boundary layer enhances and the thickness of concentration boundary layer reduces with increase in Dufour parameter (or decrease in Soret parameter).

Figs. 7-9 represent the variation of  $f'$ ,  $\theta$  &  $\phi$  with index parameter  $m$ . It is observed that the velocity component enhances with increase in  $m$ . From figs. 7 & 8 we notice that the thickness of the temperature and concentration boundary layers decrease in the flow region. Figs. 10-12 represent the variation of  $f'$ ,  $\theta$  &  $\phi$  with chemical reaction parameter  $k$ . It is observed from fig.10 that  $|f'|$  reduces in the degenerating chemical reaction case and enhances in the generating chemical reaction case with increase in  $k$ . From figs.11 & 12 we observe that the temperature and concentration boundary layers decrease in the degenerating chemical reaction case and enhance in the generating chemical reaction case.

Figs. 13-15 represent the variation of  $f'$ ,  $\theta$  &  $\phi$  for different values of suction/injection  $f_w$ . It is observed from the fig. 13 that the velocity component reduces with increase in suction parameter  $f_w$  while it enhances with increase in injection parameter  $|f_w|$ . From fig. 14 we find that the thickness of the temperature boundary layer depreciates with  $f_w$  while increase in suction parameter  $|f_w|$  leads to an enhancement in the thickness of the temperature boundary layer. From fig. 15 we notice that the actual concentration enhances with increase in  $|f_w|$ .

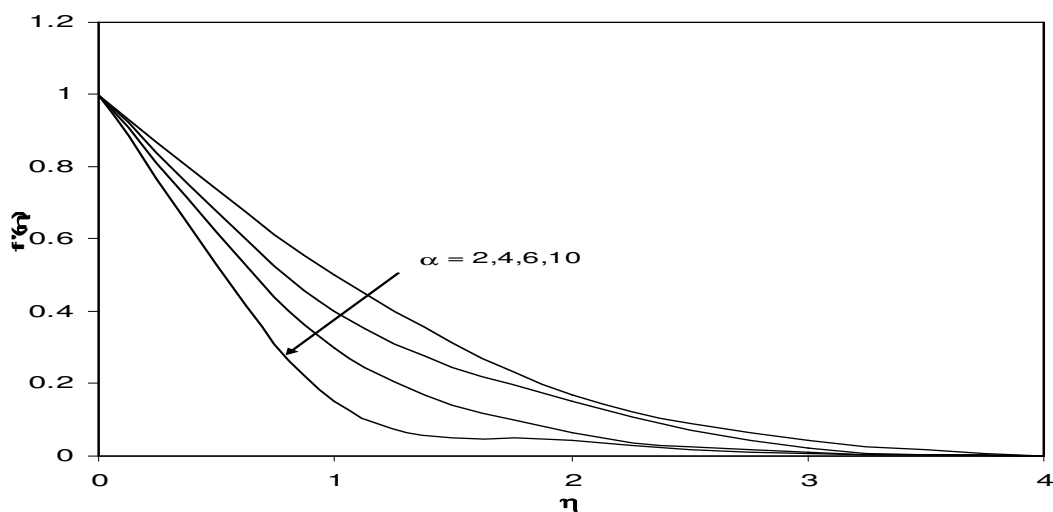


Fig. 1 Variation of  $f'(\eta)$  with  $\alpha$

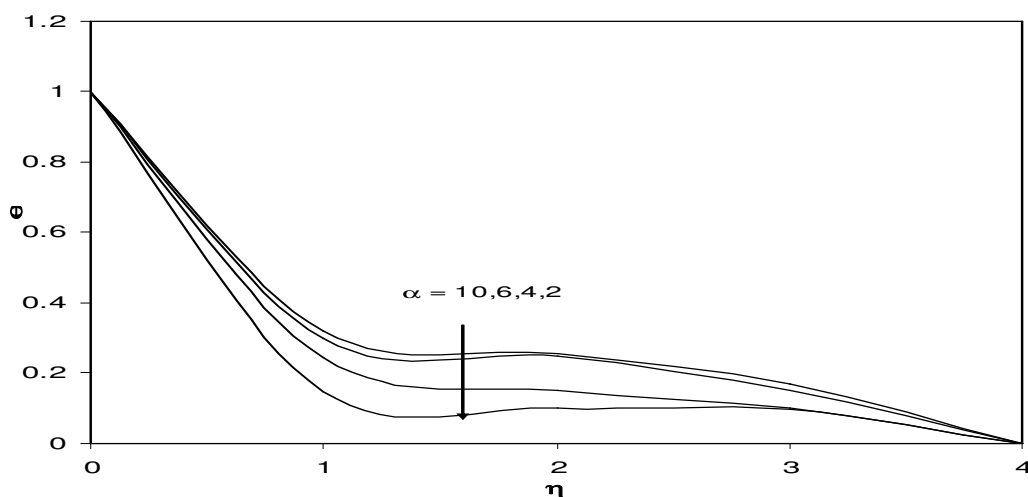


Fig. 2 Variation of  $\theta$  with  $\alpha$

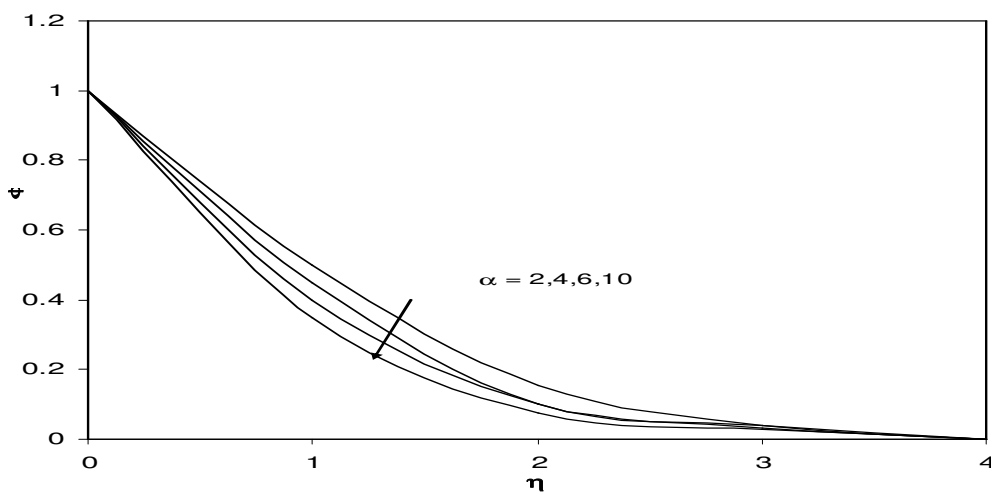


Fig. 3 Variation of  $\phi$  with  $\alpha$



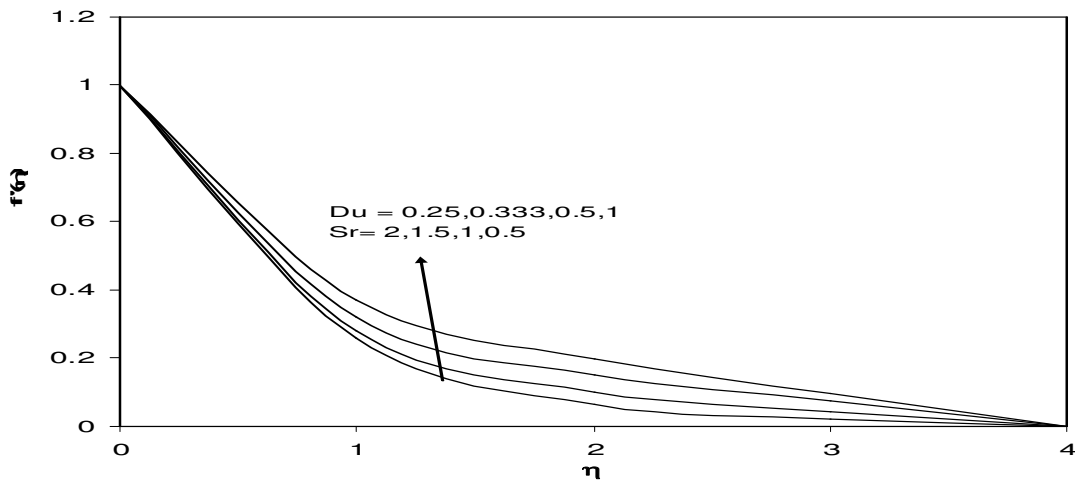


Fig. 4 Variation of  $f'(\eta)$  with  $Du$  and  $Sr$

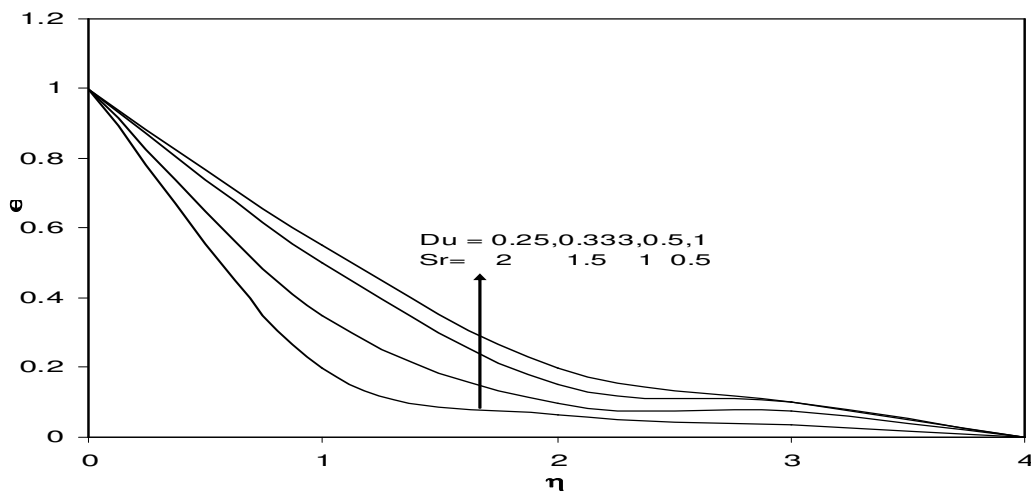


Fig. 5 Variation of  $\theta$  with  $Du$  &  $Sr$

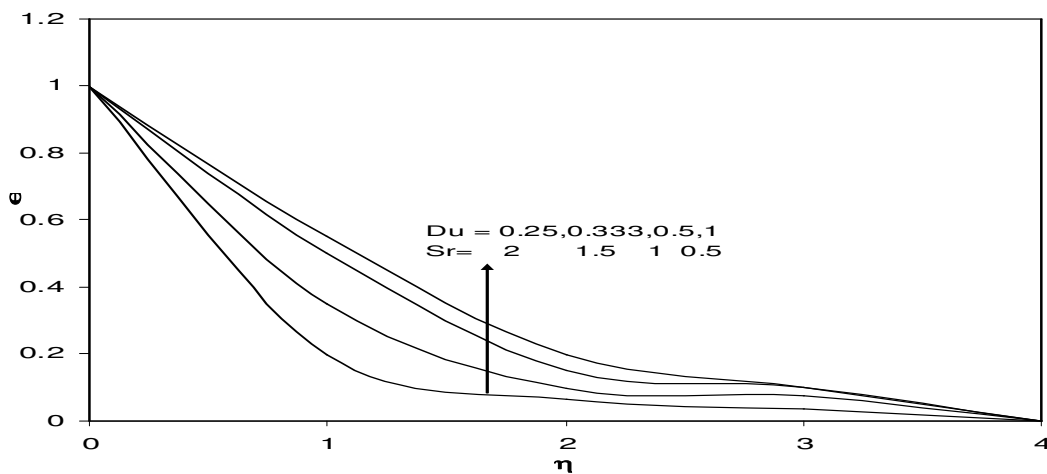


Fig. 6 Variation of  $\phi$  with  $Du$  and  $Sr$

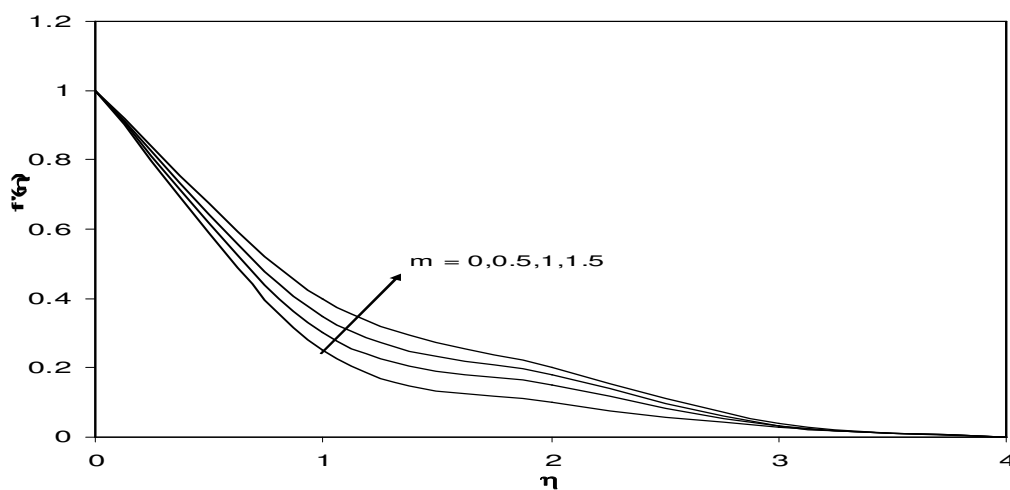


Fig. 7 Variation of  $f'(\eta)$  with  $m$

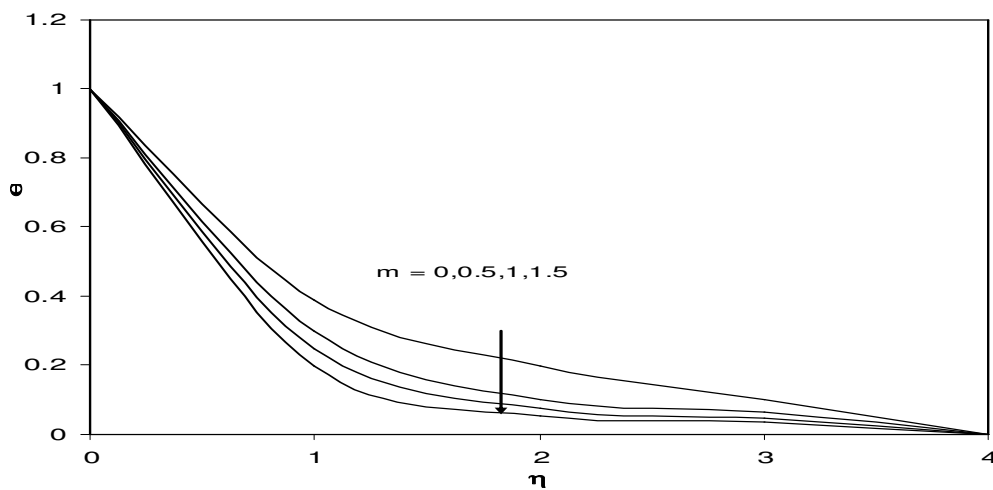


Fig.8 Variation of  $\theta$  with  $m$

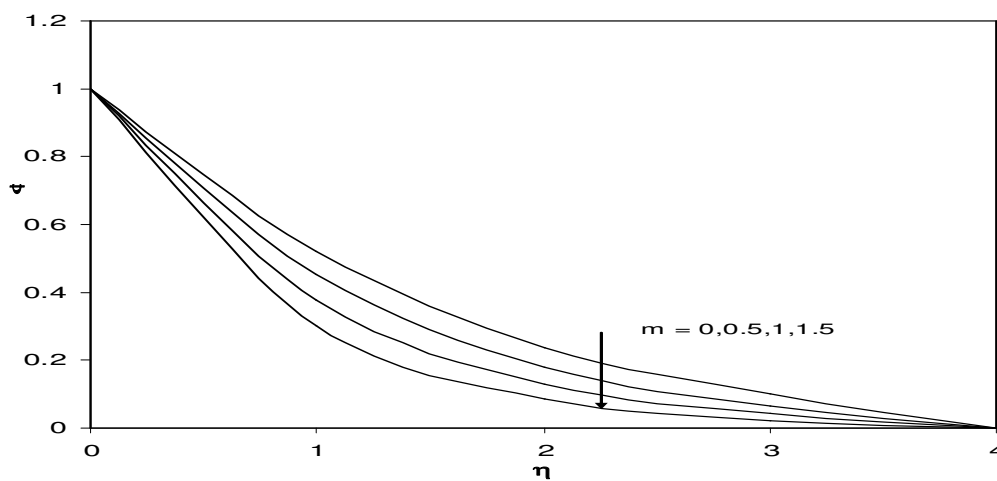


Fig. 9 Variation of  $\phi$  with  $m$

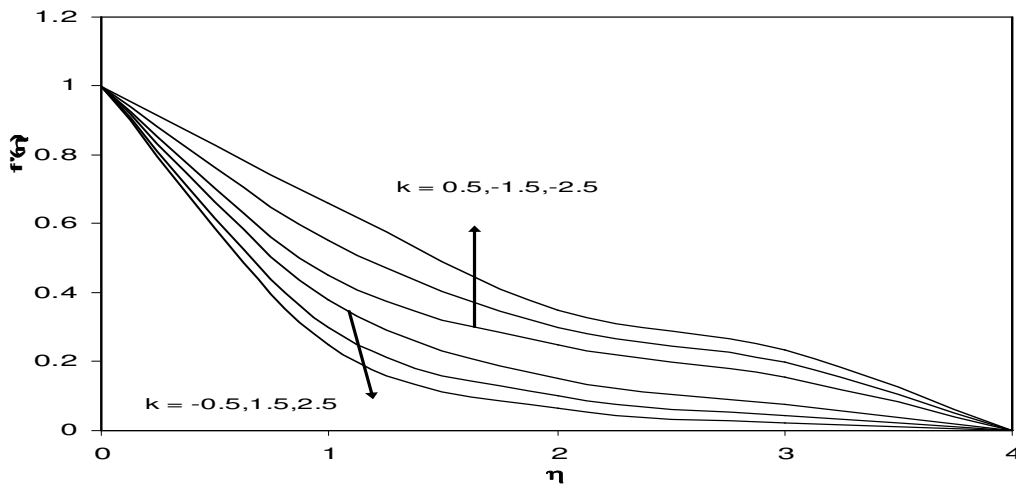


Fig. 10 Variation of  $f'(\eta)$  with  $k$

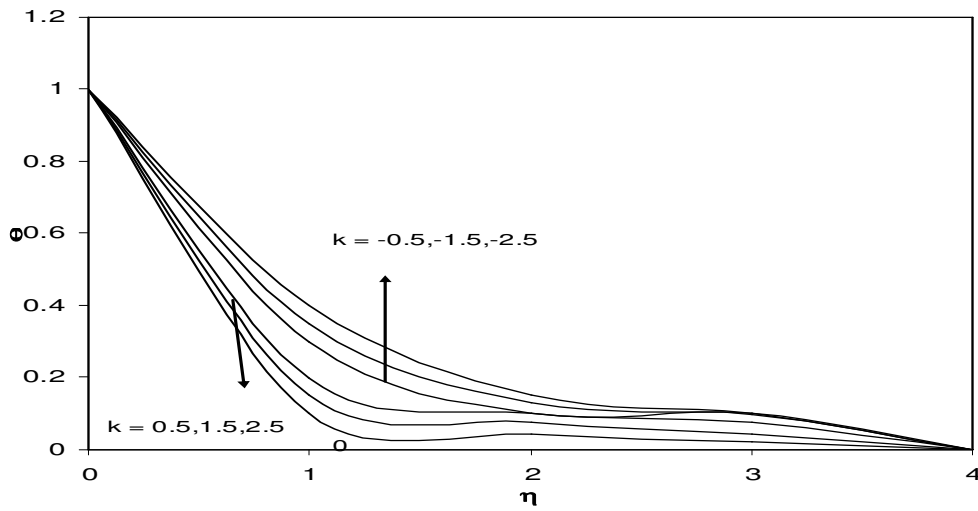


Fig. 11 Variation of  $\theta$  with  $k$

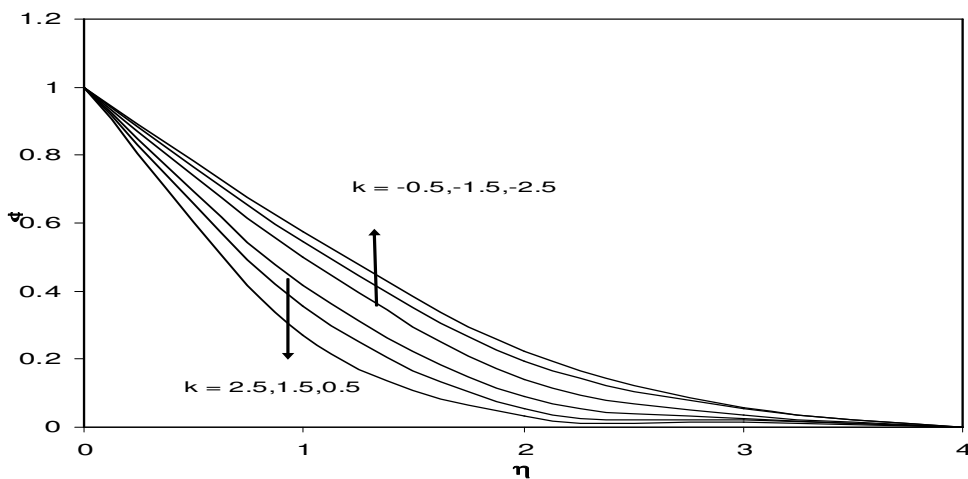


Fig. 12 Variation of  $\phi$  with  $k$

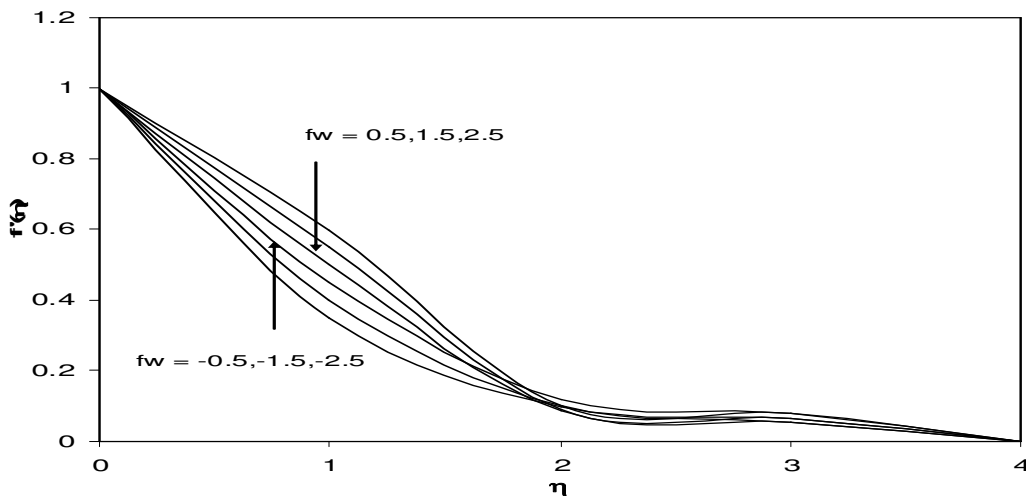


Fig. 13 Variation of  $f'(\eta)$  with  $fw$

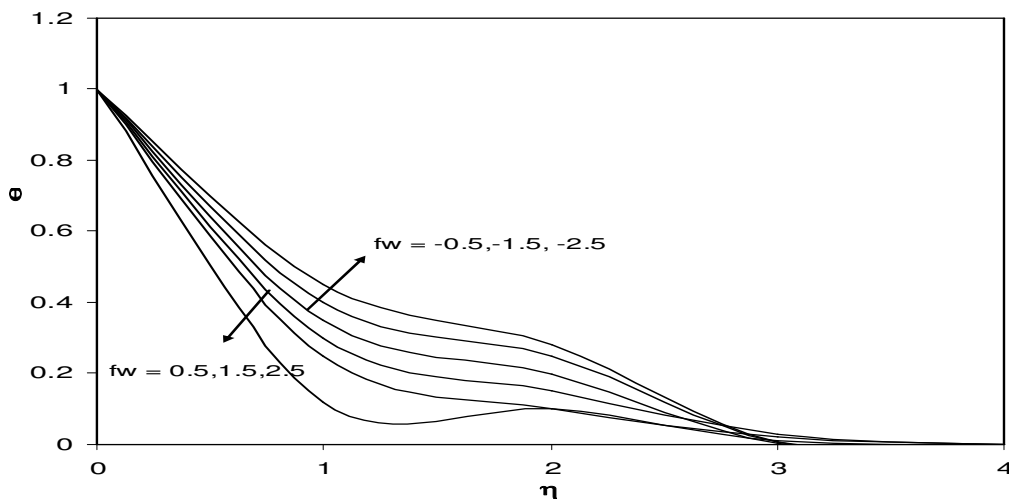


Fig. 14 Variation of  $\theta$  with  $fw$

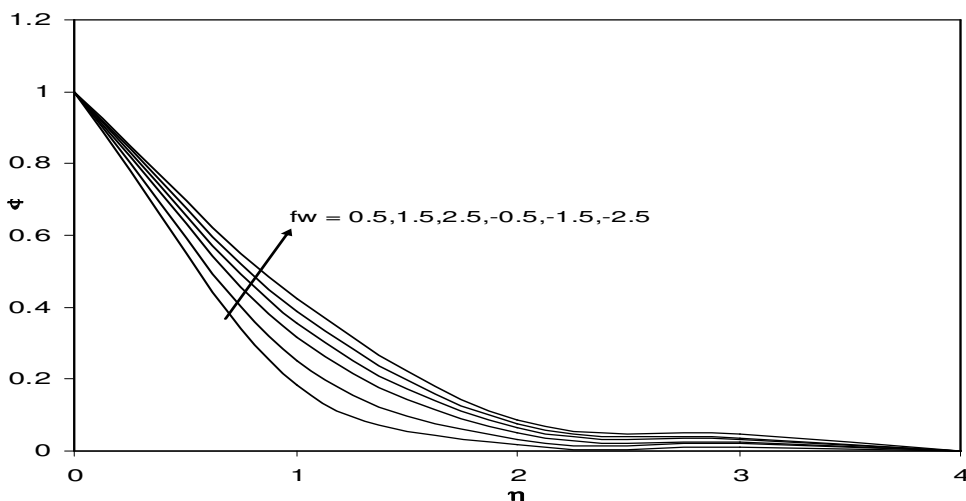


Fig. 15 Variation of  $\phi$  with  $fw$

The skin-friction ( $\tau$ ) at  $\eta=0$  is shown in tables 1-3 for different values of  $M$ ,  $Sc$ ,  $Du$ ,  $Sr$ ,  $\alpha$ ,  $k$ ,  $m$  and  $Pr$ . It is found that the skin-friction at the plate enhances with increase in the Hartman number  $M < 1.5$  and depreciates with  $M \geq 2.5$ . The variation of  $\tau$  with Schmidt number  $Sc$  shows that lesser the molecular diffusivity larger is  $|\tau|_{\eta=0}$  for all  $M$  and for further lowering of the molecular diffusivity smaller is  $|\tau|$  at the plate. With

respect to Soret parameter  $Sr$ , it can be seen that  $|\tau|$  depreciates for  $M \leq 0.5$  and enhances with higher  $M \leq 1.5$  with increase in  $Sr \leq 1$  and for higher  $Sr \geq 1$ , we notice a depreciation in  $|\tau|$  for  $M \leq 1.5$  and enhancement for  $M \geq 2.5$ . An increase in the Dufour parameter  $Du$  leads to an enhancement in  $|\tau|$  for  $M \leq 1.5$  and depreciates with  $Du$  for higher  $M \geq 2.5$ . With respect to heat source parameter  $\alpha$  we find that  $|\tau|$  depreciates with  $\alpha \leq 2$  and for higher  $\alpha \geq 4$ ,  $|\tau|$  enhances for  $M \leq 1.5$  and depreciates for  $M \geq 2.5$  (Table-1). Table-2 represents the variation of  $\tau$  with chemical reaction parameter  $k$ . It is found that  $|\tau|$  enhances for  $M \leq 1.5$  and depreciates for  $M \geq 2.5$  with increase in  $k \leq 1.5$ , while for higher  $k \geq 2.5$ ,  $|\tau|$  depreciates for  $M \leq 1.5$  with increase in  $k \geq 0$  and for higher  $M \geq 2.5$  it enhances on the plate. An increase in the index parameter  $m \leq 1$  depreciates  $|\tau|$  at  $\eta = 0$  and for higher  $m \geq 2$ ,  $|\tau|$  enhances for  $M \leq 0.5$  and depreciates with  $M \geq 2.5$ . With respect to Prandtl number  $Pr$ , we observed that the skin-friction enhances for  $M \leq 0.5$  and depreciates for  $M \geq 1.5$ . For  $Pr \leq 1$  and for higher  $Pr \geq 2$  we notice an enhancement in  $|\tau|$  for all  $M$  (Table 3).

**Table-1: Skin-friction ( $\tau$ ) at  $\eta=0$**

M	I	II	III	IV	V	VI	VII	VIII	IX
0.5	-299314	-3.26014	-3.41614	-2.93116	-2.99061	-2.93975	-2.84909	-1.37434	-3.16283
1.5	-3.0674	-3.38072	-3.78255	-3.60194	-3.67278	-3.04739	-3.08259	-1.85158	-2.69304
5.0	-1.99197	-2.45788	-3.12666	-0.90173	-2.02315	-2.09111	-2.16198	-2.73668	-2.29999
Sc	0.24	0.6	1.3	2.01	1.3	1.3	1.3	1.3	1.3
Du	0.03	0.03	0.03	0.03	0.15	0.3	0.03	0.03	0.03
Sr	0.4	0.4	0.4	0.4	0.6	1	2	0.4	0.4
$\alpha$	2	2	2	2	2	2	2	4	6

**Table-2: Skin-friction ( $\tau$ ) at  $\eta=0$**

M	I	II	III	IV	V	VI
0.5	-3.41614	-3.15434	-3.04229	-2.92208	-2.88136	-2.85371
1.5	-3.78255	-3.36668	-3.20068	-3.04071	-3.02531	-3.01401
5.0	-3.12666	-2.22051	-3.53872	-2.00507	-2.02858	-2.95976
k	0.5	1.5	2.5	-0.5	-1.5	-2.5

**Table-3: Skin-friction ( $\tau$ ) at  $\eta=0$**

M	I	II	III	IV	V	VI	VII	VIII	IX	X
0.5	-3.36167	-2.61614	-2.87864	-3.24253	-299314	-4.08074	-4.08174	-1.71008	-1.32862	-1.20782
1.5	-3.52823	-2.78255	-1.75811	-1.42858	-3.0674	-2.51877	-2.68879	-2.57788	-2.12712	-1.65988
5.0	-3.97729	-3.12666	-1.39356	-1.49981	-1.99197	-1.59096	-1.81088	-2.14275	-1.37544	-0.719319
m	0	1	2	1	1	1	1	1	1	1
Pr	0.71	0.71	0.71	1	2	0.71	0.71	0.71	0.71	0.71

The rate of heat transfer (Nusselt number) at  $\eta = 0$  is depicted in the tables 4-6 for different parametric values. It is found that the rate of heat transfer enhances with  $M \leq 1.5$ . With respect to  $Sc$  we observe that lesser the molecular diffusivity larger is the rate of mass transfer. An increase in the Soret parameter  $Sr \leq 2$  leads to an enhancement in  $|Nu|$  and for further higher  $Sr > 2$  leads to a depreciation in  $|Nu|$ . An increase in the temperature heat source parameter  $\alpha \leq 2$ , we notice a depreciation and enhances with higher  $\alpha \geq 4$  (Table 4). The rate of variation of the  $Nu$  with chemical reaction parameter  $k$  shows that  $|Nu|$  depreciates with  $k \leq 1.5$  and enhances with higher  $k \geq 2.5$ , while it depreciates in the generating chemical reaction case (Table-5). The rate of heat transfer enhances with increase in index parameter  $m \leq 1$  and depreciates with higher  $m \geq 2$ . With respect to Prandtl number  $Pr$  it can be seen that the rate of heat transfer depreciates with increase in  $Pr \leq 1$  and enhances with  $Pr \geq 2$  (Table-6).

**Table-4: Nusselt Number (Nu) at  $\eta=0$**

M	I	II	III	IV	V	VI	VII	VIII	IX
0.5	0.805123	1.03796	2.78221	0.62783	0.802003	0.755662	0.678484	0.385703	1.11399
1.5	0.673882	1.14509	2.78522	0.71746	0.646231	0.349213	0.145019	0.532384	1.57865
5.0	0.080914	2.19554	2.85417	3.07346	0.08272	0.059175	0.032566	0.704249	2.93566
Sc	0.24	0.6	1.3	2.01	1.3	1.3	1.3	1.3	1.3
Du	0.03	0.03	0.03	0.03	0.15	0.3	0.03	0.03	0.03
Sr	0.4	0.4	0.4	0.4	0.6	1	2	0.4	0.4
$\alpha$	2	2	2	2	2	2	2	4	6

**Table-5: Nu at  $\eta=0$**

M	I	II	III	IV	V	VI
0.5	2.78221	0.943906	1.94579	0.76044	0.739743	0.728126
1.5	2.78522	1.00291	1.88167	0.89236	0.0793347	0.071661
5.0	2.85417	0.12299	1.80142	0.05333	0.0526645	0.027529
k	0.5	1.5	2.5	-0.5	-1.5	-2.5

**Table-6: Nu at  $\eta=0$**

M	I	II	III	IV	V	VI	VII	VIII	IX	X
0.5	-0.119399	2.782216	0.450028	0.383053	-1.84375	0.653155	0.654155	1.30717	1.69187	-0.502899
1.5	-0.040446	2.768522	0.053628	0.286182	-2.65711	-0.039721	-0.04364	-1.39674	-1.70002	-0.885369
5.0	0.156568	2.854173	0.102313	0.745518	-0.84698	-0.007373	-0.080049	-1.49727	1.826805	1.64757
m	0	1	2	1	1	1	1	1	1	1
Pr	0.71	0.71	0.71	1	2	0.71	0.71	0.71	0.71	0.71

The rate of mass transfer (Sherwood Number) is shown in the tables 7-9 for different parametric values. It is found that the rate of mass transfer enhances with increase in  $M \leq 1.5$  and depreciates with higher  $M \geq 5$ . With respect to Sc, we find that lesser the molecular diffusivity larger is the rate of mass transfer and for further lowering of molecular diffusivity ( $Sc \geq 2.01$ ) smaller is |Sh| at  $\eta=0$ . An increase in Soret parameter  $Sr \leq 1$  leads to a depreciation in |Sh| for all M, while for higher  $Sr \geq 2$  we notice an enhancement in |Sh|. The variation of Sh with Dufour parameter Du shows that the rate of mass transfer depreciates with increase in Du. An increase in the strengths of heat generating sources results in a depreciation in |Sh| at  $\eta=0$  (Table-7). Table-8 represents variation of rate of mass transfer with chemical reaction parameter k. The variation of Sh in the degenerating chemical reaction case ( $k > 0$ ) shows that |Sh| depreciates with increase in  $k \leq 1.5$  and enhances with higher  $k \geq 2.5$ , while in the generating chemical reaction case |Sh| enhances for all M. An increase in the index parameter  $m \leq 1$  enhances |Sh| and depreciates with higher  $m \geq 2$ . |Sh| depreciates with increase in  $Pr \leq 1$  and enhances with higher  $Pr \geq 2$  (Table-9).

**Table-7: Sherwood Number (Sh) at  $\eta=0$**

M	I	II	III	IV	V	VI	VII	VIII	IX
0.5	-0.016719	-1.20205	-4.04615	-3.73408	0.13301	0.323973	0.167391	0.140782	0.123456
1.5	-0.070298	-1.74124	-4.14242	-4.11347	-0.05169	-0.087039	0.159823	0.145886	0.125678
5.0	0.06711	-0.72693	-4.54617	-2.29476	0.04997	0.081959	0.130372	0.122387	0.106584
Sc	0.24	0.6	1.3	2.01	1.3	1.3	1.3	1.3	1.3
Du	0.03	0.03	0.03	0.03	0.15	0.3	0.03	0.03	0.03
Sr	0.4	0.4	0.4	0.4	0.6	1	2	0.4	0.4
$\alpha$	2	2	2	2	2	2	2	4	6

**Table-8: Sh at  $\eta=0$**

M	I	II	III	IV	V	VI
0.5	-4.04615	-0.841769	-4.90584	0.326946	0.534072	0.692002
1.5	-4.14242	-1.37388	-5.36777	0.245887	0.470688	0.644529
5.0	-4.54617	-0.64068	-6.53652	0.375843	0.582326	0.741053
k	0.5	1.5	2.5	-0.5	-1.5	-2.5

**Table-9: Sh at  $\eta=0$**

M	I	II	III	IV	V	VI	VII	VIII	IX	X
0.5	-0.150945	-4.0465	-0.228715	-0.05374	-0.231356	-0.111398	-0.111398	0.22919	0.35909	0.171644
1.5	-0.156515	-4.1624	0.0907285	-0.10783	-0.280032	-0.003515	-0.034588	-0.14514	-0.24478	0.171289
5.0	-0.132862	-4.54617	0.101827	0.169854	0.2971196	0.001802	-0.045397	-0.04364	0.28116	0.256365
m	0	1	2	1	1	1	1	1	1	1
Pr	0.71	0.71	0.71	1	2	0.71	0.71	0.71	0.71	0.71

## 6. Conclusions

This paper presents the effects of Soret, Dufour and Chemical reaction on convective heat and mass transfer of an incompressible, electrically conducting fluid over a stretching sheet in the presence of heat generating sources. The similarity solutions are obtained by using scaling transformations. Furthermore, these similarity equations are solved numerically by using shooting technique with fourth-order Runge-Kutta integration scheme. A comparison with previously published work is performed and the results are found to be in good agreement. Numerical results of the local skin-friction coefficient, the local Nusselt number and the local Sherwood number as well as the velocity, the temperature and the concentration profiles are presented for different physical parameters. The numerical observations are as follows:

- An increase in the magnetic field parameter depreciates the friction factor and heat transfer rate.
- A raise in the heat source parameter depreciates the velocity, temperature and concentration profiles of the flow.
- An increase in Dufour number enhances the velocity, temperature and concentration profiles of the flow.
- Soret number have tendency to decrease the velocity, temperature and concentration boundary layers.
- An increase in Prandtl number depreciates the mass transfer rate.

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